

South32 Limited | ACN 093 732 597

Attachment 3B -

## Works Approval Supporting Document.

Prepared by

South32 Worsley Alumina Environmental Department

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## 

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#### **Terms and Abbreviations**

Description
Aboriginal Heritage Act 1972
Australian Height Datum
Australian National Committee on Large Dams
Boddington Bauxite Mine
Bauxite residue disposal area
Construction Quality Assurance
Controlled Residue Solids
Department of Mines, Industry Regulation and Safety
Department of Water and Environmental Regulation
Engineer of Record
Environmental Protection Act 1986
Environmental Protection and Biodiversity Conservation Act 1999
Factor of Safety
Freshwater Lake
Financial Year
Global Industry Standards of Tailings Management
Interim Biogeographic Regionalisation for Australia
Meters Australian Height Datum
Metres per second
Million tons per annum
Northern Valley Pipe Head Dam
Public Drinking Water Source Area
Pipe Head Dams including NVPHD and SVPHD
Probable Maximum Precipitation
Quality Control System
Refinery Catchment Lake
Residue Deposition Strategy
The Worsley Refinery
Rights in Water and Irrigation Act 1914
Reduced Level
Refinery Lease Area
Solar Evaporation Pond



SVPHD	Southern Valley Pipe Head Dam
TARP	Triggered Action Response Plan
The Project	Worsley Bauxite-Alumina Project
TSF	Tailings Storage Facility
The Worsley State	Alumina Refinery (Worsley) Agreement Act 1973
Agreement	
The Project	Worsley Bauxite-Alumina Project
t	Tonnes
VLW	Worsley Joint Venture
Worsley	South32 Worsley Alumina Pty Ltd



## **1** Introduction

South32 Worsley Alumina Pty Ltd (Worsley) operates the Worsley Bauxite-Alumina Project (the Project) at the Boddington Bauxite Mine (BBM), the Worsley Refinery (the Refinery) and the Port Facility at Bunbury. The Project is located 130 km southeast of Perth, approximately 15 km north-west of Collie and at the Port of Bunbury, in the South West region of Western Australia (WA) (Figure 1.1). Worsley is the manager of the operations on behalf of the Worsley Joint Venture (WJV) – Bauxite Alumina Operations. Construction of the Refinery commenced in 1980, and the first alumina was produced in April 1984.

The Project's mining, processing and associated operations are currently authorised under the *Alumina Refinery (Worsley) Agreement Act 1973* (the Agreement Act) and Ministerial Statement 719, issued under Part IV of the *Environmental Protection Act 1986* (EP Act).

The BBM is located approximately 5 km from the town of Boddington and is primarily situated on Mining Lease M258SA, granted under the Agreement Act. The Refinery is located on Crown Lease L150306. The Refinery is authorised under Part V of the EP Act, through Licence L4504/1981/17 (the Licence), to produce up to 4.7 Mtpa of alumina.

Bauxite ore mined at the BBM is crushed at crushing facilities within the mining area and then transported via an overland bauxite conveyor to the Refinery. The process of refining ore into alumina comprises a four stage Bayer Process involving digestion, clarification, precipitation, and calcination.

Residual sand and mud (bauxite residue) from the process is pumped as an alkaline slurry to the Bauxite Deposition Disposal Area (BRDA) where excess caustic and liquor is collected in pipe head dams and recycled through the process back to Refinery Catchment Lake (RCL).

Alumina produced at the Refinery is then transported by train to Bunbury Port, where it is shipped to aluminium smelters around the world.





Figure 1.1 : Location Map

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## **2** Part 2: Application Details

This Works Approval application supporting document has been prepared in support of a Works Approval application under Section 53 of the EP Act for works at the prescribed premises which may alter or increase the discharge of wastes or emissions to the environment. The Refinery is a licensed prescribed premise under Schedule 1 of the Environmental Protection Regulations 1987 for bauxite refining, including the operation of BRDAs, as defined under the Licence held by South32 Worsley Alumina Ltd.

This Works Approval application is to authorise works relating to staged 5 m lifts to BRDA 4X and BRDA 5 for financial year (FY)25. This supporting document provides technical information relevant to the application for the construction of embankments and related structures relevant to the FY25 lifts to BRDA 4X and BRDA 5 only and does not seek approval for the deposition of bauxite residue. The content of this document and additional requirements, as may be imposed by the Department of Water and Environmental Regulation (DWER), will inform the conditions for the development of and the post-construction Environmental Compliance Report and Critical Infrastructure Containment Infrastructure Report.

## 3 Part 3: Premises Details

The Refinery is located approximately 15 km north-west of the town of Collie with the primary function of processing bauxite mined from the nearby BBM into calcined alumina via the Bayer process. The Bayer process used at Worsley has the following key elements:

- Grinding Bauxite is delivered to the refinery via overland conveyor from the Boddington Bauxite operations. It then passes through a crushing/grinding circuit;
- Digestion Crushed/ground bauxite is mixed with caustic at high temperature and pressure liberating odorous volatile organic compounds;
- Clarification Washing, settlement and filtration of digested liquor (and diversion of "red mud" to BRDAs);
- Precipitation/Seed Preparation The clarified liquor is cooled and seeded with precipitation of hydrated alumina crystals;
- Liquor Burning Liquor and oxalate streams are passed through a high-temperature furnace to remove dissolved organic material and destroy oxalate. Solar Evaporation Ponds (SEPs) that have been converted into temporary oxalate storage dams;
- Calcination Dehydration of hydrated alumina in high-temperature furnace to produce calcined alumina (a fine white powder); and
- Bauxite Residue Disposal Area Residual sand and mud (bauxite residue) from the process is pumped as an alkaline slurry to the residue drying area where excess caustic and liquor is collected and recycled through the process.

This process results in the production of emissions and discharges that classify the Refinery as a prescribed premise requiring authorisation under Part V of the EP Act. Schedule 1 of the Environmental Protection Regulations 1987 describes the activities that require licensing.

Table 3-1BRDA 5 construction began in 1994, with a 30 m high starter embankment along the west perimeter, followed by subsequent upstream raises in 2001 (Stage 2), 2005 (Stage 3), 2009 (Stage 4), and 2014 (Stages 5). BRDA 5 stands approximately 52 m high and was built using an upstream method.



Stage 6B was partially constructed in FY23 but it is not yet operational. The expected closure date for BRDA 5 is 2050.

Table 3-1 provides a list of the approved prescribed activities under the Licence that are undertaken at the Refinery.

Table 3-1: Prescribeo	activities	under Licence	L4504/1981/17
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Prescribed premises category description (Schedule 1, Environmental Protection Regulations 1987)	Assessed production / design capacity
Category 46: Bauxite refining	4.7 million tonnes (t) per annual period assessed production capacity
Category 52: Electric power generation	260 Mega Watts per annual period design capacity
Category 53: Flyash disposal	110,000 t per annual period assessed production capacity
Category 54: Sewage facility	270 cubic metres per day design capacity
Category 61: Liquid waste facility	100 t per annual period assessed production capacity
Category 63: Class I Inert landfill site	15,000 t per annual period assessed production capacity
Category 89: Putrescible landfill site	500 t per annual period assessed production capacity

The Refinery has two areas where BRDAs are currently in operation. To the north of the Refinery, within the Northern Valley BRDAs are: BRDA 1; BRDA 2, BRDA 4 (cells 1 & 2) and BRDA 4X (cells 1 & 2 have been merged) and to the south of the Refinery lies the Southern Valley BRDA which consists of BRDA 5 (Cells 1 - 7). The Worsley BRDA operations are located within the boundary of the Refinery Lease Agreement (Figure 3.1). A more detailed layout of BRDA's 4X and 5 are provided in Figure 3.2 and Figure 3.3.

BRDA 4X construction began in 1999 as an extension to BRDA4, following a similar design concept to BRDA 4, and Stage 5 has been completed. It is currently an average height of 45 m, and the upstream raise method was used. BRDA 4X was initially divided into three cells, however, over time, the number of partitions was reduced to one cell during the construction of Stage 5. Decant towers collected liquor and rainwater from the surface of the residue and discharged to the Northern Valley Pipe Head Dam (NVPHD) via a buried pipeline located just below the BRDA west embankment. The expected closure date for BRDA 4X is 2030.

BRDA 5 construction began in 1994, with a 30 m high starter embankment along the west perimeter, followed by subsequent upstream raises in 2001 (Stage 2), 2005 (Stage 3), 2009 (Stage 4), and 2014 (Stages 5). BRDA 5 stands approximately 52 m high and was built using an upstream method. Stage 6B was partially constructed in FY23 but it is not yet operational. The expected closure date for BRDA 5 is 2050.



In addition, the following key structures form part of the BRDA operations:

- Northern Valley Pipe Head Dam (NVPHD): All residue and groundwater underdrains from Northern Valley BRDAs discharge by gravity to the NVPHD. The NVPHD collects rain runoff, decant liquor, and groundwater underdrain discharges, and pumps the combined "process water" to the RCL.
- Southern Valley Pipe Head Dam (SVPHD): All residue and groundwater underdrains from Southern Valley BRDAs discharge by gravity to the SVPHD. The SVPHD collects all underdrain discharges and pumps them to the RCL via sump.
- Solar Evaporation Ponds (SEPs): Temporary storage of oxalate is provided through SEPs. SEPs include SEP1, SEP2A, SEP3 and SEP4. Water Body 1 (WB1): This facility is primarily used for the storage of excess residue liquor that accumulates in the wet season and provides water balance along with SEP2A to RCL.
- Refinery Catchment Lake (RCL): The RCL receives residue liquor from the NVPHD, the SVPHD and the BRDAs as well as Refinery process water. It is equipped with pumps and piping to transfer excess residue liquor to WB1 / SEP2A and to return the residue liquor to the Refinery.
- Freshwater Lake (FWL): The FWL has a roughly rectangular shaped main water body and north and south arms that extend northeast and southwest up the northern and southern valleys, respectively. The north and south arms extend to just below the NVPHD and SVPHD, respectively. The lake stores clean run- off water from the water diversion trenches, and the surface run-off from the Northern Valley and Southern Valley BRDA embankments. The embankment outer slope runoff does not contact process water and reports directly to the FWL.



Figure 3.1: BRDA Layout within Refinery Lease Area





Figure 3.2: BRDA 4X Current Layout



Figure 3.3: BRDA 5 Current Layout



The hazard class for both BRDAs has been assessed under the Australian National Committee on Large Dams (ANCOLD), Department of Mines, Industry Regulation and Safety (DMIRS) and Global Industry Standards of Tailings Management (GISTM) as described in Table 3-2.

#### Table 3-2: Hazard Class

BRDA	ANCOLD	DMIRS	GISTM
4X	High B	Category 1 (High Hazard)	Very High
5	High B	Category 1 (High Hazard)	Very High

An ANCOLD rating, of "High B" consequence category dams is defined as potentially 10 to 100 people at risk, with potentially "major" severity level impacts (\$100m - >\$1B damage cost, depending on BRDA and potential for consequential failure).

The DMIRS classification is based on the maximum embankment or structure height being greater than 15 m and the high significance of impact to life and/or property due to failure or uncontrolled release (DMP, 2013).

In regard to the GISTM ratings, the BRDAs classification of 'Very High' consequence category dams means very high economic losses affecting important infrastructure or services and high relocation/compensation to communities < US\$1B.)

Advanced technical studies completed by third parties and validated by International Experts have validated that BRDAs at Worsley are well managed and constructed to a high standard. The bauxite residue is well compacted to required strength and density using Amphirollers with good water management practices to allow for future raises using upstream construction.

Geotechnical studies that would support a stability assessment prior to the commencement of deposition are currently in progress. Once all stability assessments have been completed and peer reviewed by suitably qualified subject matter experts, Worsley will submit the audit reports to DWER and commence deposition.



## **4 Part 4: Proposed Activities**

#### 4.1 Design Overview

The proposed scope of works outlined in this section are for FY25. BRDA 4X Stage 6 will require the construction of a 5 m embankment raise to RL 309 mAHD along the eastern BRDA 4X perimeter (Figure 4.1). BRDA 5 Stage 6A also consists of a 5 m embankment raise to RL 290.5 mAHD to the north, east and southern perimeter of Cell 6 (Figure 4.2). The raises incorporate a number of components which are identified in Table 4-1.

#### Table 4-1: Scope of Construction Works FY25

BRDA 4X Stage 6	BRDA 5 Stage 6A	
Upstream embankment construction (northern and western perimeter)	Partial centerline construction (northern perimeter)	
Downstream embankment construction (eastern perimeter)	Partial downstream embankment construction (northern perimeter)	
Partial upstream construction (4/4X dividing wall)	Upstream embankment construction (southern and eastern perimeter)	
Extending decant tower (No. 1, 2 &3)	Capping of existing Decant Towers	
Decant access causeway into BRDA 4X	Re-position decant access causeway into Cell 6 (Figure 4.2)	
Operational access for inspection and maintenance	Construct Amphiroller ramps	
Storm water runoff features from perimeter embankments.	Storm water runoff features from perimeter embankments	
	Operational access for inspection and maintenance	
	Direct operational pond to the west of the cell, outside of the structural zone (Figure 4.2)	





Figure 4.1: BRDA 4X Stage 6 Proposed Configuration





Figure 4.2: BDRA 5 Stage 6A Proposed Cell 6 Configuration

4.2 Proposed Staging of Embankments and Raises

#### 4.2.1 BRDA 4X

BRDA 4X Stage 6 will be predominately constructed as an upstream embankment raise (constructed on residue). Monitoring of embankment settlement during construction will be via settlement plates installed prior to construction of the upstream lift (LOM, 2023a).

The typical BRDA 4X Stage 6 embankment cross sections are shown on Figure 4.3. Embankment modifications to Stage 6 (relative to Stage 5) and the corresponding reason/justification for each modification are presented in Table 4-2.

	Table 4-2 :	Embankment	Modification	n and Justific	ation
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Embankment Modification	Justification
Drop Structure	Drop structure in Stage 6 with spacing 150 m. The functionality of toe drainage and drop structures and limit remediation works required over the life of operations and at closure, spacing between drop structures is limited to 150 m in length.





Figure 4.3 : BDRA 4X Stage 6 Section View

The Construction Quality Assurance (CQA) is managed onsite under the control of the BRDA Construction Superintendent. The CQA program has been developed over the 34-year life of the BRDAs. In addition, an independent NATA registered soils testing laboratory is located onsite, specifically for CQA testing of earthwork materials. No major changes are proposed to the current CQA program for BRDA 4X Stage 6. The earthworks specification has been developed by Worsley over the life of the BRDAs, into a comprehensive document, and has been updated by Worsley for the FY25 construction season. The control/management of deviances in construction and testing tolerances is managed by Worsley (LOM, 2023a).

The analysis of residue strength and BRDA stability undertaken as part of the Going Higher Study (AECOM, 2018) has confirmed that the BRDAs can be safely constructed to an elevation of a reduced



level (RL) 345mAHD, or higher if required, limited only by considerations of practical construction and operation of smaller cell areas as the height increases. Using conservative strength parameters, the factor of safety against dam wall instability exceeds current industry guidelines for both operational and closure performance (LOM, 2023a).

#### 4.2.2 BRDA 5

BRDA 5 Stage 6A will be predominantly constructed in an upstream configuration around the southern and eastern perimeter. The northern perimeter of Cell 6 will be a combination of centreline embankment raise (310 m) and downstream embankment raise as shown in Figure 4.4 (LOM, 2023b).



Figure 4.4 : BDRA 5 6A Plan

Embankment features of the Stage 6A raise and the corresponding reason/justification for each feature, as identified by LoM (2023b), are presented in Table 4-3. The typical Stage 6A embankment cross sections for upstream, downstream and centerline are shown on Figure 4.5 to Figure 4.7.



#### Table 4-3: BRDA 5 Stage 6A Embankment Features and Justification

Embankment	Justification	
Progressive closure batter	The BRDA 5 Stage 6A progressive closure batter has been designed to include a "hinge point" approximately 1.5 m above the Stage 5A crest road with the slope above the hinge point being slightly steeper than the slope below the hinge point. This also serves to ease the transition into the new toe drain (spoon drain) detail. Due to the parallel work in Cell 7, only the southern embankment of Cell 6 is covered with the closure batter at this stage.	
Toe drain modified from 5C v- drain to shallow 4C spoon drain.	A modified toe drain (spoon drain) detail has been developed to replace the typical v-drain detail for drainage grades <3%. The modified toe drain comprises a spoon drain which is a continuation of the crest road (Zone 4C gravel) to accommodate low flows off the embankment and crest road to the drop structure.	
Sand fingers from 16 m to 32 m on upstream raise	Sand finger spacing at Stage 6A southern embankment has been increased from 16 m to 32 m (upstream raise) in line with the spacing of the upstream toe drainage system which will carry on for subsequent lifts. No sand finger in eastern upstream embankment (Cell 6/7 Splitter Bund), spacing on the downstream constructed portions of the Stage 6A raise remain unchanged.	
Sand finger protection	Recent experience has shown that surface water flow off the embankment crests has caused damage to the sand fingers, requiring significant repair. To protect the sand fingers and embankment crest edge from erosion, the upstream crest edge windrow will remain in place at the sand finger locations. The steel mudline will serve as a Light Vehicles (LV) barrier where no windrow is present.	
Upstream toe drainage system	The intent of the upstream toe drainage system is to assist in reduction of pore pressures within the deposited residue near the embankment to increase the Factor of Safety (FoS) for slope stability of future raises. It needs to be noted that there is no internal drainage pipe in Cell 6 eastern embankment.	
Elimination of zoned downstream embankment	Material testing of the Zone 1A and Zone 2A material showed no discernible difference between the two materials. The two- zone embankment design has been modified in favour of a single zone (homogenous) design of Zone 2A material for downstream construction. (LOM, 2023b)	





Figure 4.5: Typical Section - Downstream Embankment



Figure 4.6: Typical Section - Upstream Embankment





Figure 4.7: Typical Sections - Centerline Embankment

The embankment drainage system for BRDA 5 up to and including the Stage 6A consists of sand fingers on the upstream embankment (400 mm thick by 4m wide) and downstream/centreline embankment batters (400 mm thick by 4 m wide).

A key condition to achieving an acceptable FoS for the potential final height of RL 345 mAHD or higher is to maintain the design pore water pressures. For BRDA 5 this requires an upstream toe drainage system to allow pore pressures within the residue nearest the perimeter embankment to dissipate. The upstream toe drainage system will comprise slotted polyvinyl chloride (PVC) drains surrounded by gravel and wrapped in geotextile. The drains will extend 50 m from the upstream toe of the embankment; approximately three per 100 m of embankment. Should excess pore pressures be generated, the drainage pipework would collect seepage and convey it through perforated pipe (PVC pipe) within the filter/drain and via closed pipework to the BRDA 5 floor drain (Figure 4.8).

No upstream toe drainage system or sand fingers will be installed in the eastern embankment Cell 6. A toe drainage system will be installed at Stage 8 when the embankment is at a sufficient height to outlet directly to the Cell 7 Decant Pond (LOM, 2023b).

CQA for BRDA 5 is managed onsite under the control of the BRDA Construction Superintendent. No major changes are proposed to the current CQA program for BRDA 5 Stage 6A. The earthworks specification has been developed by Worsley over the life of the BRDAs, into a comprehensive document, and has been updated by Worsley for FY25 construction season. The control/management of deviances in construction and testing tolerances is managed by Worsley.





Figure 4.8: Upstream Toe Drain

Table 4-4: General Tailings Properties

#### 4.3 Tailings Properties and Deposition

For the effective deposition of tailings, Worsley have set a minimum solids content target of 55% percentage of weight (wt). From past experience, a 54% solids content affects the beach angle development, the decant pond size and the dewatering cycle times and Amphiroller passes. On the other hand, exceeding 58% (wt) solids content can impose limitations within the refinery with respect to pumping (particularly to BRDA 4X, which is 30 m higher than BRDA 5). Testing of minimum solids content between November 2015 to February 2016 yielded an averaged 55.7% (wt) solids content, with a range of 52.6% to 59.1% (wt) (LOM, 2023b).

Property	Description

Property	Description
Tailings type	Non-settling thickened tailings, 10.5 Mtpa (1,250 tons per hour).
Pump pressure at Geho pump	8500 kPa through 2 x 250 mm diameter steel mud lines (typical)
Initial solids content	55% (average – measured daily via nuclear density meter on discharge pipe) at nominally 100 to 200 centipoises



Property	Descriptior	ı				
Final solids content	72% (minimum – measured via survey, monthly and in situ annually) and 28kPa shear strength (target minimum). Note: solids content assumes -2% soda: 74% with soda included					
Time to reach 72% solids content:	30 days in s amphirollin only	30 days in summer, 60 days in winter, annual average 42 days with amphirolling. 18 months without amphirolling in upper 1.5m crust only				
Soil classification:	Sandy SILT	Sandy SILT				
Specific gravity:	3.65 to 3.90	), average 3.78				
Dry density:	1.56 to 1.86	, t/m <sup>3</sup>				
Voids ratio, e₀:	1.09 - 1.31					
Plasticity index:	4 to 10%, av	4 to 10%, average 7%				
Beach angle:	0.6% but varies daily based on depth of pour (suction of underlying desiccated residue), on plasticity index and solids content- determined by monthly laser scanning of active cells.					
Rate of rise:	1.7m/year					
Permeability:	1x10 <sup>-6</sup> m/s o	on deposition decreasing to 5x10 <sup>-8</sup> m/s at 72% solids.				
Soda content of deposited residue:	2.03% (Jan 2	2000 to August 2009, based on liquor density)				
pH of deposited residue:	12.3					
	9.5mm	100%				
	4.75mm	99%				
Particle size distribution: (Jan 2016 average):	1.18mm	98%				
	0.425mm	88%				
	0.075mm	60%				

Tailings deposition at BRDA 4X and BRDA 5 are managed by a team of engineers and technicians, under the direction of the Worsley Engineering Manager. No changes are proposed to the operation of the BRDAs 4X and BRDA 5, as a result of construction of BRDA 4X Stage 6 and BRDA 5 Stage 6A respectively. The following points are of relevance to the design process:

- Spigots are managed four-hourly around the cell perimeter in areas of short pours and overnight in areas of significant beach length, to maintain the pond around the decant. The design of regular shaped cells is therefore preferred from an operability viewpoint.
- A beach length of around 500 m has been found to be about optimum with 55% solids content, which



forms a 0.6-degree beach slope.

- As part of the mud deposition strategy at Worsley, Amphirollers are used to plough the residue surface until a minimum undrained shear strength of 28 kPa is achieved for each layer. This is tested opposite every discharge spigot around the full perimeter of each cell, at 50 m out from the embankment, and recorded as a performance target; the 28 kPa shear strength approximating a final solids content of 72%.
- For handover to construction for the next stage, the shear strength of the final 1 m (top 1 m) must be a minimum of 100 kPa (now changed to 70 kPa by Worsley in 2020) to avoid bearing capacity failure during construction of the upstream raise. Shear strength testing via handheld vane shear will be undertaken prior to construction to confirm that minimum shear strength requirements have been met.
- The in situ vane shear strength of the mud is tested by Worsley's G&TS's civil engineer prior to commencement of construction, in order to verify that the required mud strength has been achieved. The scope of this testing is outside of this design report.

Extensive monitoring of the performance of the BRDAs wall stability and water management is conducted and includes:

- Daily and weekly surface and embankment inspections;
- Drone surveys: Pond size & location; deposition performance and beach slopes;
- Satellite surveys that can measure < 5 mm disturbances in the embankments;
- Piezometer readings of pore pressure in embankments; and
- Full depth residue samples to verify residue strength.

Before each of the 5 m upstream raises are initiated, measures are implemented to ensure that the deposited residue has sufficient strength to support the planned raise. Tailings strength is achieved by the drying and consolidation of deposited tailings through a combination of installed drainage systems, evaporation through wind and sun action, and active compaction and drying methods using GPS tracked Amphirollers/mud farming, dozer plowing and compaction to achieve a controlled residue solids (CRS) percentage. This is especially important where an upstream embankment raising method is used, as this method consists of the construction of new, raised retaining embankments on consolidated tailings.

#### 4.4 Construction Quality Assurance

#### 4.4.1 CONSTRUCTION QUALITY CONTROL SYSTEM

Worsley has established a Quality Control System (QCS) that is applicable to the construction of the BRDA 4X Stage 6 and BRDA 5 Stage 6A lifts. The relevant objectives of the QCS are to ensure that:

- All sections of the works are completed in accordance with the Drawings, Specification and any specific Site Instructions;
- Material quality and compaction standards are met;
- Zone material thickness, pipe placement and other construction tolerances are adhered to;
- Rework is minimised;
- Relevant key performance indicators are agreed, monitored and reported to all personnel employed on the project works;
- There is continuous improvement in the practical and collaborative application of the QCS; and
- The construction equipment, methodology and layer thicknesses adopted in the Contractor's method statement are recorded in the Annual BRDA Construction Report.

#### 4.4.2 CONSTRUCTION QUALITY ASSURANCE REQUIREMENTS

Specific measures relating to the quality assurance of upstream raise embankment construction



shall include:

- In advance of construction, a method statement shall be finalised that will detail the equipment used to place and compact the embankment, as well as planned lift thicknesses and the planned minimum number of passes of the compaction equipment for each lift;
- Compaction control techniques, including the taking of sampling and testing methodologies shall be in accordance with the requirements of AS 1289, as set out in the BRDA Earthworks Specification;
- A risk-based change management procedure, including the written amendment of the method statement, will be implemented where the need for changes are identified;
- The offset at each compacted lift of the embankment shall be marked along the edge as construction progresses;
- Layer depth sampling and testing by a Materials Testing Laboratory shall be conducted as specified in the BRDA Earthworks Specification;
- A minimum of three (3) nuclear density tests (one (1) test on each side of the embankment and one (1) random location) shall be performed for each lift per construction bay. The maximum length of a construction bay shall be 200 m; and
- All materials used for construction shall be in strict accordance with the requirements of the BRDA Earthworks Specification, manufacturer's recommendations and the Worsley BRDA Civil Engineer's written instructions.

#### 4.4.3 POST-CONSTRUCTION SIGN-OFF

Once construction is complete, a construction report is prepared detailing all construction works and technical queries if raised. The report is signed by Engineer of Record (EOR) and the Worsley Accountable Executive to validate that the design intent was met during construction.

#### 4.5 Storage Capacity

As per the recent survey data (as of June 2023) provided, a summary of the storage capacity for all BRDAs and waterbodies is given in Table 4-5. For this Works Approval application, the relevant cells for BRDA 4X and BRDA 5 are highlighted.



#### Table 4-5: BRDA Storage Capacity as of June 2023

BRDA	Avg. toe (m AHD)	Operational freeboard (m)	Beach slope (avg.) (%)	Remaining deposition capacity to design surface (m <sup>3</sup> )	Remaining deposition capacity to freeboard for 1 in 1000 AEP storm (m <sup>3</sup> )	PMP volume (m <sup>3</sup> )	Remaining deposition capacity to freeboard for 6 hr PMP (m <sup>3</sup> )
BRDA 2, S8	312.07	2.36	-1.31	1,206,378	1,109,427	-	1,352,530
BRDA 4, S7(Cell 1)	297.65	7.38	-0.83	4,367,569	4,235,814	556,181	4,565,631
BRDA4, S7(Cell 2)	298.03	7.26	-0.66	4,131,151	4,009,696	498,013	4,356,306
BRDA 4X, S5	300.69	5.24	-0.79	4,397,930	4,224,440	791,881	4,700,015
BRDA 5, S5B (Cell 1)	288.24	1.01	-0.95	318,548	500,926	306,304	684,334
BRDA5, S5B (Cell 2)	285.57	2.25	-0.68	757,773	1,087,278	412,009	1,418,955
BRDA5, S5B (Cell 3)	284.66	1.32	-0.84	361,490	574,619	365,701	812,799
BRDA5, S5B (Cell 4)	286.24	2.11	-0.66	208,395	348,971	335,745	548,429
BRDA5, S5B (Cell 5)	284.84	1.42	-0.93	973,195	1,164,254	539,201	1,508,931
BRDA5, S5A (Cell 6)	283.22	3.13	-0.85	1,580,885	1,851,962	504,954	2,183,531
BRDA5, S4A (Cell 7)	280.04	6.81	-0.75	2,084,745	2,191,840	268,442	2,364,788



## **5** Part 7: Other Approvals and Consultation

#### 5.1 Alumina Refinery (Worsley) Agreement Act 1973

Worsley currently operates under the *Alumina Refinery (Worsley) Agreement Act 1973* (Worsley State Agreement). The Worsley State Agreement provided the initial basis for the Project to proceed. Clause 5A of the Worsley State Agreement Act required the RWJV to submit a detailed Environmental Review and Management Programme (ERMP) for assessment and approval in order for the Project to begin. Reporting against the sections c5A(3) & section c16(10) of the Worsley State Agreement Act is undertaken annually through submission of the Worsley 10-Year Plan and Annual Review process.

#### 5.2 *Mining* Act 1978

BRDA 4X and BRDA 5 are governed under Crown Lease Agreement I154246, which effectively covers three separate areas inside the RLA. The western portion of the RLA is overlaid by part of Mining Lease M258SA, thus permitting mining activity within the overlapping zone.

The design, construction, operation and closure of all tailings storage facilities (TSF) in Western Australian mines must comply with the *Mines Safety and Inspection Act 1994*, *Mines Safety and Inspection Regulations 1995* and *Mining Act 1978* as well as DEMIRS' codes and guidelines. Annual BRDA Audits are conducted by independent third parties and submitted to DEMIRS to ensure compliance with the following DEMIRS guidance:

- Code of Practice: Tailings storage facilities in Western Australia;
- Guide to Departmental requirements for the management and closure of TSF; and
- Tailings storage facility audit.

#### 5.3 Part IV Environmental Protection Act 1986

Ministerial Statement 719 applies to the Refinery and the associated BBM. In relation to the current application, Worsley is required to implement the Water Resource Management Plan for the protection and management of nearby proclaimed water resources and to give effect to a zero discharge to these natural resources, and thereby not diminish their environmental value or use.

The Refinery operations were assessed in a 2005 application which was subsequently approved under Ministerial Statement 719 (and several subsequent Section 45C applications and approvals). The Refinery has an approved production rate of 4.7 Mtpa. Schedule 1 of Ministerial Statement 719 includes management limits for SO<sub>2</sub>, NOx, Particulates and VOC's. These air emissions and associated targets and reporting are also currently regulated through the Environmental Protection Licence (L4504/1981/17) issued under Part V of the EP Act.

#### 5.4 Environment Protection and Biodiversity Conservation Act 1999

In June 2004, Worsley's proposal to increase the production rate at the Refinery from 3.5 Mtpa to 4.4 Mtpa ("Worsley Alumina Efficiency and Growth"), included five additional mining areas: East Quindanning, Morgan's, Hotham North Extension, Central and Brookton, was assessed under the *Environment Protection and Biodiversity Conservation Act 1999* (EPBC Act) through the Bilateral Agreement between the Commonwealth and the State of Western Australia. EPBC Act approval 2004/1566 was issued for the "Worsley Alumina Efficiency and Growth" aspects of the Project on 6 June 2007.



## 6 Part 9: Emissions, discharges and waste

The following potential emissions and discharges have been identified in relation to the proposed FY25 construction works.

#### 6.1 Surface Water

BRDA 4X is located approximately 800 m north-east of FWL which feeds into the Augustus River. Surface water management features are in place to separately collect fresh water and residue impacted water and convey these separate streams to the FWL and RCL respectively. Construction activities will be conducted to ensure surface water flows from BRDA 4X flows via gravel lined spoondrains at the toe of the embankments leading to rock-lined drop structures to the base of BRDA. From the base of BRDA 4X, surface water then reports to the NVPHD (Figure 6.1). The flow capacity of the main diversion channels around the BRDAs has previously been designed, by others, for a 6-hour Probable Maximum Precipitation (PMP) event.



Figure 6.1: BRDA 4X Surface Water Management

BRDA 5 is located approximately 650 m south-east of FWL which feeds into the Augustus River. The FWL receives rainwater falling on the outside batters of BRDA 5, which is classed as forming part of the Refinery's clean water circuit. Water falling on the outside slopes is unaffected by bauxite residue and is therefore directed to the FWL via silt traps to intercept clayey silt that may be entrained from flowing over the outside batters. Construction activities will be conducted in a manner that promotes the drainage of rainwater falling on the construction areas to its upstream side, i.e. onto the BRDA. This is achieved by the establishment of a construction bund on the downstream edge of the construction area and by inclining embankment layers and road surfaces to the upstream side.



Surface water flow from BRDA 5 Stage 6A will be via gravel lined spoon-drains at the toe of the Stage 6A embankment leading to rock-lined drop structures to the base of BRDA 5. From the base of BRDA 5, surface water will report to the diversion drain through the southern valley silt trap and into the southern arm of the freshwater lake. The flow capacity of the main diversion channels around the BRDAs has previously been designed, by others, for a 6-hour PMP event, leading to significant overcapacity compared to the TSF Code of Practice (DMP, 2013) of a 1 in 100-year average return interval event.

Water monitoring at FWL is conducted monthly and includes parameters such as pH, EC, dissolved oxygen, turbidity, temperature, sodium chlorine and aluminium, as defined in the Water Management Plan (South32, 2021). In the event that adverse water quality from either BRDA is detected or exceedance of a trigger level occurs, a Trigger Action Response Plan (TARP) is activated. Actions from the implementation of the TARP will, amongst other action, include an investigation into the source of the exceedance and will implement corrective actions to address the cause and effects, if any.

FY25 construction activities performed outside the footprint of the BRDA, such as the loading and transport of construction materials, also have the potential to cause contamination of surface water, primarily through accidental releases of contaminants, such as hydrocarbons, and through the siltation of surface water flows. Accidental releases of hydrocarbons and other pollutants are managed under the Refinery's spill response and clean-up procedures. The potential siltation of surface water flows that may report to natural receptors, such as FWL and the Augustus River, is managed through on-site water drainage arrangements and the routing of water via sedimentation ponds before it is released to the FWL.

With the established management and monitoring procedures in place, it is highly unlikely that the construction activities for FY25 will result in poor water quality reaching the FWL. Surface water monitoring locations are shown in Figure 6.2.

#### 6.2 Groundwater

Both BRDAs have low permeability clay liners that cover the entire footprint with under drainage systems to protect underlying groundwater from seepage from the residue areas via a network of underflow collection pipes. The underdrainage systems provide a defense against seepage to the groundwater by substantially lowering the hydraulic head at the base of the BRDA's deposit. Groundwater monitoring is currently undertaken below the BRDAs to detect changes in water quality in accordance with Ministerial Conditions in Ministerial Statement 719. Monitoring locations are shown in Figure 6.2. No impacts to groundwater from the BRDA operations have been detected to date. Waste processing and containment infrastructure for the BRDAs are also managed in accordance with the Licence L4504/1981/17.

Liquor from the active deposition areas is drained to the closed liquor circuit via the decant system and the internal drains located around the inside perimeter of the BRDAs. Seepage of water from embankment raise activities performed as part of the FY25 works will therefore be captured by the above-mentioned liquor collection and drainage system and will be prevented from coming into contact with groundwater.

Construction activities performed outside the footprint of the BRDA, such as the loading and transport of construction materials, also have the potential to cause contamination of groundwater, primarily through the accidental releases of contaminants, such as hydrocarbons. These are managed under the



Refinery's spill response and clean-up procedures.

The Refinery operates an extensive groundwater monitoring network, which comprises upstream reference bores, potential impact bores in the immediate vicinity and down gradient of potential contamination sources, as described in the Water Management Plan (South32, 2021). Data is compared to historic data for the site and specific trigger levels for each bore. In the event of an adverse trend or exceedance of a trigger level the TARP is activated.

Given the nature and size of the existing operations, it is unlikely that any material contamination to groundwater will occur during the construction of the BRDA 5 FY25 embankment raise.





Figure 6.2: Refinery Surface and Groundwater Monitoring Locations

6.3 Air Emissions and Dust

The BRDAs surface tends to dry out as the weather warms and rainfall decreases later in the year. As wind speeds traditionally increase through October/November, the potential of BRDA dust liberation



increases dramatically. To suppress dust, the BRDAs surface will be hydromulched with the addition of Gluon 500 polymere to increase resistance to summer rain events and sustained strong winds.

Dust may also be generated during the construction of the FY25 embankment raise from the loading, transport and delivery of construction materials, through construction plant and vehicle movements and through physical earthworks. Water carts will be used as required during the construction phases to assist with the management of fugitive dust. Other management strategies that are employed at Worsley to manage dust on the BRDAs include the use of surface binding agents and the use of dust suppressant where required. Much of the potential for dust generation with be avoided by adherence to construction material moisture requirements.

The management of dust emissions during construction works at the BRDA will continue to be carried out in alignment with the draft Air Quality and Dust Management Plan – RLA (Attachment 8D). The Refinery conducts ongoing investigations into the use of different dust controls in the BRDA areas, including the use of a combination of dust suppressant, surface binding agents and ripping of the BRDA surfaces. Fixed dust monitoring stations are installed on the Refinery boundary (Figure 6.3). Two Tapered Element Oscillating Microbalances and one E-Sampler, targeting particulate matter with a diameter of 10 microns (PM<sub>10</sub>) particles, are used to monitor dust impacts from the BRDAs, roads, tracks and construction areas (including material handling) at the Refinery. PM<sub>10</sub> particles are monitored according to the National Environment Protection Measures – Ambient Air Quality Standard and are reported in Worsley's Annual Environmental Report (AER). No exceedances due to BRDA activities have been recorded at sensitive receptors. Worsley will continue to track and investigate complaints made from the community in relation to dust in accordance with the Worsley Community Complaint Procedure.





Figure 6.3: Dust Monitoring Locations and Sensitive Receptors



## 7 Conceptual Site Model/Risk Assessment

The key emissions and associated actual or likely pathway during premises construction and operation which have been considered are detailed in Table 7-1 which also details the control measures the applicant has proposed to assist in controlling these emissions, where necessary. The Conceptual Site Model/Risk Assessment is applicable for BRDA 4X and BDRA 5.

Table 7-1: Conceptual Site Model (CSM) table for BDRA 4X and BRDA 5

Source / Activities	Potential emissions, pollutants, or contaminants of concern	Potential pathway	Potential receptors	Potential impacts	Proposed controls and contingencies
Construction					
Transport, mixing, compaction of materials for the construction of embankments, internal causeways, splinter bunds, construction ramps, vehicle movements, lift-off from stockpiles and/or stored product, earthworks etc.	Dust	Air/ windborne pathway	Single rural dwelling approximately 6 km due south and north of premises	Health and amenity impacts	Water carts. Surface binding agents. Adherence to construction material moisture requirements. Cessation of a particular operation or an amendment to operational procedure when dust cannot be controlled. Air Quality Management Plan
	Noise	Air/ windborne pathway	Single rural dwelling approximately 6 km due south and north of premises	Health and amenity impacts	All onsite machinery compliant with vehicle noise emission requirements. Site will conduct works in accordance with Section 4 of AS 2436- 2010 Guide to Noise and Vibration Control on Construction, Demolition and Maintenance Sites (standards Australia 2010) Separation distances are such that any noise and vibration from construction works is sufficient that will not occur
Mobilisation of stormwater	Sediment laden runoff. Potentially contaminated stormwater	Overland runoff	Augustus River approximately 2km north west of the BRDAs	Reduced surface water quality and ecosystem disturbance.	Outside batters of BRDA 4X and BRDA 5 are captured by toe drains, diversion culverts to the FWL via silt traps. Construction of a bund on the downstream side of the construction areas so that loose materials subject to mobilisation to stormwater runoff will be undertaken such that the drainage of rainfall falls to the upstream side of embankments where possible. Water quality monitored within the FWL include parameters for turbidity. If a trigger level is exceeded, as defined in the sites TARP, an investigation into the source of the exceedances and implementation of corrective action will occur to address the cause of the incident.
Embankment failure (Dam Break)	Bauxite residue Slurry water: containing Al <sub>2</sub> O <sub>3</sub> , Na <sub>2</sub> , CO <sub>3</sub> , and SO <sub>4</sub>	Direct discharge and overland flow to nearby land and water	Augustus River approximately 2km north west of the BRDAs. Native vegetation in State Forest	Reduced surface water quality and ecosystem disturbance. Reduced vegetation health and potential loss of vegetation in some areas.	The construction methods determine the capacity of the embankments to remain stable under a range of conditions during operations. Construction will occur in accordance with the Life of Mine Design Report BRDA 4X – Stage 6 Raise (2023), Life of Mine Design Report BRDA 5 – Stage 6A Raise (2023); and the premises CQA Plan. The Works Approval Holder provides that these reports demonstrate the embankment raise is compliant with the: • Code of Practice for Tailings Storage Facilities (DMIRS); • Australian National Committee on Large Dams (ANCOLD);



Source / Activities	Potential emissions, pollutants, or contaminants of concern	Potential pathway	Potential receptors	Potential impacts	Proposed controls and contingencies
Onerstiens					<ul> <li>Guidelines on Tailings Dam Planning Design, Australian National Committee on Large Dams (ANCOLD); and</li> <li>Guidelines on Dam Safety Management (ANCOLD, 2003).</li> <li>The Design Report BRDA 4X - Stage 6 Raise (2023) and Design Report BRDA 5 - Stage 6A Raise (2023) contain an assessment of the Stability of the dams under seismic loading, drained and undrained conditions. The report claims the BRDA 5 when constructed to the above specifications, will meet the minimum factors of safety. Deposition will not commence until these claims have been verified by an independent assessment through a third party geotechnical assessment of the Design Report and until any critical issues identified through the third party review, are satisfactorily addressed.</li> </ul>
Operations					
Embankment failure (Dam Break)	Bauxite Residue Slurry water: containing Al <sub>2</sub> O <sub>3</sub> , Na <sub>2</sub> , CO <sub>3</sub> , and SO <sub>4</sub>	Direct discharge and overland flow to nearby land and water	Augustus River approximately 2km north west of the BRDAs. Native vegetation in State Forest	Reduced surface water quality and ecosystem disturbance. Reduced vegetation health and potential loss of vegetation in some areas.	<ul> <li>Management of water within the raise prior to deposition mass being consolidated is through careful management of tailings deposition and supernatant in accordance with the BRDA Operating Maintenance and Surveillance Manual:</li> <li>Daily inspections of BRDAs</li> <li>Delivery mudline fitted with dropper pipe spigots that minimise velocity of deposition;</li> <li>Spigots paced an average of 72 m apart and managed 4-hourly short pours around perimeter embankments to maintain pond around the decant tower;</li> <li>Beach length of approximately 500 m with tailings deposition of 55% solids and a 0.6% degree beach slope;</li> <li>Wet pours of a maximum of 1.1 m at a time; and</li> <li>Use of Amphirollers on wet pours within 72hours of pour until an undrained shear strength of 28 kPa is achieved for each layer.</li> </ul>
Leaks and spills from pipelines, mudlines, pumps and associated infrastructure	Bauxite residue, and decant water Slurry water: containing Al <sub>2</sub> O <sub>3</sub> , Na <sub>2</sub> , CO <sub>3</sub> , and SO <sub>4</sub>	Direct discharge and overland flow to nearby land and water	Augustus River approximately 2 km north west of the BRDAs	Reduced groundwater quality and impacts to downgradient groundwater users.	<ul> <li>Comprehensive and daily monitoring of BRDA's including mudlines delivering bauxite to the BRDA's, decant recovery pipelines and valves;</li> <li>Scheduled maintenance;</li> <li>Incident recording and reporting</li> <li>TARP to identify and respond to issues as they arise;</li> </ul>



Source / Activities	Potential emissions, pollutants, or contaminants of concern	Potential pathway	Potential receptors	Potential impacts	Proposed controls and contingencies
					<ul> <li>The site is operated as a closed system, contaminated water and leachate from spills is contained within the premises; and</li> <li>Extensive groundwater and surface monitoring is undertaken to validate effectiveness of controls (under Ministerial Statement 719).</li> </ul>
Overtopping of BRDA due to excess loading or heavy rainfall events or both	Bauxite residue, and decant water Slurry water: containing Al <sub>2</sub> O <sub>3</sub> , Na <sub>2</sub> , CO <sub>3</sub> , and SO <sub>4</sub>	Overland flow, direct discharge to soil, infiltration to groundwater	Augustus River approximately 2km north west of the BRDAs. Native vegetation in State Forest	Reduced surface water quality and ecosystem disturbance. Reduced vegetation health and potential loss of vegetation in some areas.	<ul> <li>Maintenance of operational freeboard of 0.5 m between the tailings at the top of the beach and the embankment crest (inclusive of wave action);</li> <li>The beach angle over 100 m of beach is 0.6 m;</li> <li>Only two or three cells are actively used at any one time, may be used in the event of an extreme storm event to temporarily store storm water;</li> <li>Maximum operating levels are calculated to only be exceeded in a 1:1,000 year annual recurrence interval storm event;</li> <li>Ability to move contaminated storm water following high rainfall events to other containment infrastructure on site such that a water from an extreme 1: 1000- year annual rainfall incidence 72 hour duration event is completely contained within the premises infrastructure, enabling compliance with the sites "zero discharge" requirements under the Agreement Act; and</li> <li>TARP to identify and respond to issues as they arise.</li> </ul>
Seepage of contaminants through the base of the BRDA liner causing groundwater contamination and mounding	Leachate Slurry water: containing Al <sub>2</sub> O <sub>3</sub> , Na <sub>2</sub> , CO <sub>3</sub> , and SO <sub>4</sub>	Direct discharge to soil, infiltration to groundwater	Shallow aquifer discharging to FWL and Augustus River	Reduced groundwater quality and impacts to downgradient groundwater users.	<ul> <li>Inspection of underdrain at pipe head dam inflow;</li> <li>Report any changes</li> <li>Vacuum pumping to unblock pipes if required;</li> <li>TARP to identify and respond to issues as they arise;</li> <li>The site is operated as a closed system, contaminated water and leachate is contained within the premises; and</li> <li>Extensive groundwater and surface monitoring is undertaken to validate effectiveness of controls (under Ministerial Statement 719).</li> </ul>
Contaminated stormwater run off	Mobilisation of stormwater	Overland flow, direct discharge to soil, infiltration to groundwater	Shallow aquifer discharging to Freshwater Lake and Augustus River	Reduced surface water quality and ecosystem disturbance.	<ul> <li>Design such that stormwater that falls on the downstream side of perimeter embankments is diverted to of Gravel lined spoon drains at the toe of embankment leading to rock drops;</li> <li>The rock drops report to southern diversion dam through southern valley silt trap to the southern arm of the FWL; and</li> <li>Periodic testing of FWL is undertaken.in accordance with</li> </ul>



Source / Activities	Potential emissions, pollutants, or contaminants of concern	Potential pathway	Potential receptors	Potential impacts	Proposed controls and contingencies
					Ministerial Statement 719.
Dry deposition surface	Dust lift off	Air / windborne pathway	Nearby vegetation, nearby Augustus River approximately 2 km northwest of the BRDAs	Reduced vegetation health and potential loss of vegetation in some areas.	<ul> <li>Dust from the BRDA's is managed in accordance with the sites Air Quality and Dust Management Plan – RLA Business Blueprint and includes:</li> <li>Daily visual monitoring of BRDA surface;</li> <li>Dust monitoring stations upstream and downstream to monitor dust lift off;</li> <li>Addition of dust suppression and surface binding agents hydro mulch and Gluon500 to control dust over residue deposition areas according to BRDA annual Dust Management Plan;</li> <li>Use of water carts and sweeping in dry weather;</li> <li>Mechanical ploughing and ripping of BRDA surfaces; and</li> <li>Trigger levels and corrective action response and reporting.</li> </ul>



## 8 Monitoring and Reporting

Given that the proposed construction networks are covered by the existing Refinery surface water, groundwater and dust monitoring networks, no additional monitoring is proposed in respect to discharges to the environment.

Project inputs, including the use of fuel, lubricants and concrete will be monitored in accordance with existing Worsley procedures to facilitate sustainability reporting.

## **9 Progressive Closure**

BRDA design will incorporate progressive closure planning by integrating the ultimate closure plan within the design, construction and operation activities, and in accordance with learnings identified and trialled during recent raise designs and construction.

The progressive closure approach for future BRDA raises will build off the current BRDA closure approach where the external batter slopes are progressively closed as part of the embankment raising process.

The top surface of the BRDA will be capped when the final design heights are reached as detailed in BRDA Life of Operation Plan Study (LOM, 2020).

## **10 Part 10: Siting and Location**

#### 10.1 Climate

The Refinery is located in the southwest of WA which has a Mediterranean climate with a predominance of winter rainfall. The average maximum and minimum temperatures generally follow seasonal patterns of cold winters and hot summers. The average temperature during the summer months ranges from 12°C to 32°C and during the winter months ranges between 4°C to 17°C.

The mean monthly rainfall is low in the summer months and increases during the winter months, with rain days varying from six days in December to 21 days in July (ETA, 2020). The maximum monthly rainfall is recorded in July and August. Average rainfall records reflected higher rainfalls in the Refinery when compared to the BBM, which is located further to the east (Mattiske, 2021a).

Prevailing winds are from the east-south-east to south-south-east during summer, and from the westsouth-west to west-north-west during the winter months (ETA, 2020). Wind speeds are typically calmer during winter and increase during summer. Average wind speeds generally remained below 10 metres per second (m/s) during both winter and summer, with minimal occurrences of wind speeds exceeding 10 m/s.

#### **10.2 Landscape**

The Refinery is located on the Darling Plateau, which developed on the Archean crystalline rocks of the Yilgarn Craton. The Craton is a stable shield area, comprising linear belts of metamorphosed sedimentary and volcanic rocks that have been intruded with granitic rocks (granitoid formation). The Refinery also occurs in the Avon Province spanning the Western Darling Range soil-landscape zones. The Western Darling Range Zone is described as moderately dissected lateritic plateau on granite with deeply incised valleys. Soils are formed in laterite, lateritic colluvium, granite weathered in-situ and gneiss. Soils are formed in laterite colluvium or granite weathered in-situ (Schoknecht et al., 2004).

#### **10.3 Biodiversity**

#### 10.3.1 FLORA AND VEGETATION

The Refinery is located within the Jarrah Forest bioregion and Northern Jarrah Forest subregion as described by the Interim Biogeographic Regionalisation for Australia (IBRA). The Northern Jarrah Forest subregion is characterised by Jarrah-Marri forest on laterite gravels, and in the eastern part, by woodlands of Wandoo-Marri on clayey soils (Williams and Mitchell, 2001).

A total of 289 nine species from 54 families and 150 genera have been recorded from flora and vegetation surveys in and around the Refinery. One conservation significant species, *Pultenaea skinneri* (Priority 4), has been historically recorded as occurring within the Refinery based on the database search results. Three conservation significant flora species; *Gastrolobium* sp. Prostrate Boddington (Priority1), *Isopogon* sp. Canning Reservoir and *Senecio leucoglossus* (Priority 4) have a high likelihood of occurrence, but have not been recorded from surveys (Mattiske, 2021b).

The proposed BRDA raises do not require the clearing of vegetation and therefore will not have an impact to threatened and/or priority flora species or Threatened Ecological Communities.

#### 10.3.2 FAUNA

Numerous fauna surveys have been conducted in and around the Refinery area over the past 20 years with the most recent surveys completed in 2021 (BIOSTAT, 2021).

There are 11 conservation significant species that have either been observed or are highly likely to occur within the Refinery area. These are:

- Forest Red-tailed Black Cockatoo (Vulnerable);
- Baudin's Black Cockatoo (Endangered);
- Carnaby's Black Cockatoo (Endangered);
- Peregrine Falcon (Other specially protected species);
- Blue-billed Duck (Priority 4);
- Rakali (native water rat) (Priority 4);
- Quenda (Priority 4);
- Western Brush Wallaby (Priority 4);
- Brush-tailed Phascogale (Conservation Dependent fauna);
- Western Ringtail Possum (Critically Endangered); and
- Quokka (Vulnerable).

No clearing of vegetation is required for the FY25 BRDA raise program, therefore, no threatened and/or priority fauna or fauna habitat will be disturbed or impacted.

**10.4 Hydrology** 

#### 10.4.1 SURFACE WATER

The BRDAs are located adjacent to the Harris River Dam Catchment Area, which is classed as a Priority 1 (P1) Public Drinking Water Source Area (PDWSA). The Refinery and BRDAs run along the western boundary of the P1 area but are not located within the proclaimed catchment area. The BRDAs are located in the proclaimed Surface Water Area (Brunswick River and Tributaries) under the *Rights in Water and Irrigation Act 1914* (RIWI Act), specifically in the Leschenault Estuary – Lower Collie Area. The

BRDAs also fall within the Collie River Irrigation District which is proclaimed under the RIWI Act (South32, 2022).

The RLA lies within the Augustus River catchment, a tributary of the Brunswick River which is primarily used for agricultural purposes. The FWL at the Refinery was built in 1983 with the primary purpose of supplying fresh water to the Refinery. Surface water is managed through the South32 Water Management Plan (Attachment 8C) and is monitored at the location shown in Figure 6.2.

#### 10.4.2 GROUNDWATER

Three main aquifers have been identified within the vicinity of the Project. These have formed as a result of in-situ weathering of basement rocks and include a shallow aquifer (shallow weathered zone), a lower saprolite aquifer (deep weathered zone) and a fractured bedrock aquifer. Topography influences groundwater levels in all aquifers, with depths ranging from 1-3 m in low-lying areas to 15-40 m in higher areas. Several major watercourses and associated tributaries originating from the east dissect the Darling Plateau. Water quality varies from fresh to saline due to intermittent drainage (South32, 2022).

All aquifers remain localised and no locally significant abstraction from these aquifers is known to occur. Groundwater is managed through the South32 Water Management Plan (Attachment 8C) and is monitored at the locations shown in Figure 6.2.

#### **10.5 Heritage**

The Refinery occurs within the Gnaala Karla Booja Agreement Area of the South West Native Title Settlement. The Refinery Area has been subject to numerous targeted Aboriginal heritage surveys (both archaeological and ethnographic) over the life of the Refinery with the most recent in 2020 (Brad Goode & Associates, 2020).

There are 17 archaeological 'Other Heritage Places' that have identified within the RLA. These are classified as 'Stored Data/Not a Site' heritage places and are predominantly artefact scatters. These sites either have insufficient evidence or information to be assessed under the *Aboriginal Heritage Act 1972* (AHA) or do not meet the criteria for protection as an Aboriginal heritage site under the AHA. Of the 17 'Other Heritage Places' that occur within the RLA, five of these places are located within presently disturbed areas and no longer exist (South32, 2022). The remainder of the sites are no longer considered sites by the Aboriginal Cultural Material Committee.

There will be no impact to Aboriginal Heritage as no additional clearing is required for the FY25 BRDA raises.

## **11 Part 11: Submission of Any Other Relevant Information**

#### **11.1 Stakeholder Consultation**

Worsley Alumina have informed DWER of the planned raises for FY25 and provided them with a presentation outlining the schedule and works program. DWER are awaiting the Works Approval application so that the FY25 raises can be assessed.

#### **11.2 Additional Information**

The following documents have been provided for further information for the Works Approval application:

- Attachment 8A Design Report: BRDA 4X Stage 6;
- Attachment 8B Design Report: BRDA 5 Stage 6A;
- Attachment 8C Water Management Plan;
- Attachment 8D Air Quality and Dust Management Plan RLA; and
- Attachment 8E GISTM Requirement 15.1 Public Disclosure Worsley Alumina.

## **12 Part 12: Category checklist(s)**

#### **12.1 Tailings Storage Facilities**

As of February 2023, DWER require applications for tailings storage facilities (TSFs) (new or amended) to be provide the additional supporting forms to be submitted with the Licence and Works Approval application form. The TSF application Category Checklist (IR-F28) is mandatory for all Category 5 prescribed premises that include one or more TSFs. The Category Checklist (tailings storage facility) outlines additional information requirements for the works approval, to:

- construct and operate new TSFs; or
- amend an instrument granted for an existing TSF (i.e. new TSF cells or wall rises or lifts or changes to delivery processes or material characteristics).

The completed Category Checklist (IR-F28) is provided as Attachment 9 of this application.

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